14452-75-6; GaH, 13572-92-4; GeH, 13572-99-1; AsH, 12628-08-9; $\mathrm{BrH}, 10035-10-6$; Be, $7440-41-7$; B, 7440-42-8; C, 7440-44-0; N , 17778-88-0; $\mathrm{O}_{2}, 17778-80-2 ; \mathrm{Na}, 7440-23-5 ; \mathrm{Mg}, 7439-95-4 ; \mathrm{Al}, 7429-$ 90-5; Si, 7440-21-3; P, 7723-14-0; S, 7704-34-9; Cl, 22537-15-1; K, 7440-09-7; $\mathrm{Ca}, 7440-70-2$; Ga, 7440-55-3; Ge, 7440-56-4; As, 7440-38-2; $\mathrm{Se}, 7782-49-2$; $\mathrm{Br}_{2}$, 10097-32-2; HOCl, 7790-92-3; SeH, 13940-22-2; $\mathrm{BeH}_{2}, 7787-52-2 ; \mathrm{BH}_{3}, 13283-31-3 ; \mathrm{CH}_{4}, 74-82-8 ; \mathrm{CH}_{3} \mathrm{CH}_{3}, 74-84-0$;
$\mathrm{CH}_{2}=\mathrm{CH}_{2}, 74-85-1 ; \mathrm{CH} \equiv \mathrm{CH}, 74-86-2 ; \mathrm{HCN}, 74-90-8 ; \mathrm{CH}_{2} \mathrm{O}, 50-00-$ $0 ; \mathrm{CHO}, 2597-44-6 ; \mathrm{CH}_{3} \mathrm{~F}, 593-53-3 ; \mathrm{CO}_{2} \mathrm{H}, 64-18-6 ; \mathrm{CH}_{3} \mathrm{OH}, 67-56-1$; $\mathrm{NH}_{3}, 7664-41-7$; $\mathrm{HNC}, 6914-07-4$; $\mathrm{HNO}, 14332-28-6 ; \mathrm{HNO}_{2}$, $7782-$ 77-6; $\mathrm{HNCO}, 75-13-8 ; \mathrm{H}_{2} \mathrm{O}, 7732-18-5$; HOCN, 420-05-3; HOCHO, 64-18-6; $\mathrm{MgH}_{2}, 7693-27-8 ; \mathrm{AlH}_{3}, 7784-21-6 ; \mathrm{SiH}_{4}, 7803-62-5 ; \mathrm{PH}_{3}$, 7803-51-2; $\mathrm{SH}_{2}, 7783-06-4 ; \mathrm{GeH}_{4}, 7782-65-2 ; \mathrm{AsH}_{3}, 7784-42-1 ; \mathrm{SeH}_{2}$, 7783-07-5.

# Molecular Modeling of the Physical Properties of the Alkanes 

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#### Abstract

Eight physical properties (boiling points, molar volumes, molar refractions, heats of vaporization, surface tensions, melting points, critical temperatures, and critical pressures) of 74 normal and branched alkanes were examined by molecular modeling techniques. Structural parameters employed include Wiener indices, connectivity indices, ad hoc descriptors, information indices, and molecular volumes and surface areas. Most of the properties were well modeled ( $r^{2}>0.97$ ) by the Wiener indices, connectivity indices, and ad hoc descriptors. An exception was the melting points, which were not well modeled by any of the available indices. Factor analysis (principal component analysis) was used to examine the intrinsic dimensionalities of the data and parameter sets. A single factor accounts for about $82 \%$ of the variance in the eight physical properties, two factors account for $94 \%$, and three factors account for about $99 \%$. The melting points load strongly on a factor independent of the other properties. Of the examined parameter sets, the connectivity indices exhibited the highest dimensionality.


It is obvious that the structure of a compound, both geometric and electronic, determines its properties. Nonetheless, elucidation of the connection between molecular structure and bulk properties has posed a challenge to chemists for more than a century. A central issue has been how to quantify the elusive concept of "structure". In early attempts properties were commonly represented as sums of contributions from atoms, bonds, or larger structural subunits. ${ }^{1-7}$ These approaches often required a large number of empirical parameters, and recently attention has turned to the use of more general structural parameters, in particular those derived from chemical graph theory. ${ }^{8-15}$ Among the most successful of these general parameters have been Wiener distance indices, ${ }^{16-19}$ connectivity indices, ${ }^{9,13-15,20}$ information indices, ${ }^{12,21}$

[^0]and ad hoc descriptors. ${ }^{15,22}$ In some cases molecular volumes and surface areas have also been suggested as important variables, most notably for solubility properties. ${ }^{23-29}$

The alkanes represent an especially attractive class of compounds as a starting point for the application of molecular modeling techniques. Many properties of the alkanes vary in a regular manner with molecular mass and extent of branching, and because the alkanes are nonpolar, a number of complexities that arise with more polar compounds are avoided. Our purposes in the present report are threefold. First, we hope to obtain practical structure-property equations for eight representative physical properties of the alkanes, utilizing relatively simple structural parameters. Such equations can be used to predict values for as yet unmeasured properties of compounds and also, in some cases, may aid in the "design" of compounds with properties suitable for special purposes, Second, we wish to evaluate the relative performances of the above descriptor sets in relating the alkane molecular structures to the set of physical properties. Third, we hope to draw inferences from our results concerning the natures of the physical forces responsible for the properties observed. As an aid in this last effort, we have utilized the technique of factor analysis to estimate the inherent dimensionality of the set of physical properties investigated and also the dimensionalities of the parameter sets.

## Methods

Data. Eight representative physical properties were selected, based in part on their perceived importances and in part on the availability of a suitable body of data: boiling points (bp), molar volumes at $20^{\circ} \mathrm{C}$ (MV), molar refractions at $20^{\circ} \mathrm{C}$ (MR), heats of vaporization at $25^{\circ} \mathrm{C}$

[^1](HV), critical temperatures (TC), critical pressures (PC), surface tensions at $20^{\circ} \mathrm{C}(\mathrm{ST})$, and melting points (mp). Values for most properties were taken from ref 30 , but some values were obtained from other sources. ${ }^{31-34}$ Molar volumes were calculated as MW/d, where MW is the molecular weight and $d$ is the density $\left(\mathrm{g} / \mathrm{cm}^{3}\right)$ at $20^{\circ} \mathrm{C}$. Molar refractions were calculated from the index of refraction $n_{0}, \mathrm{MV}$, and $d$, using the Lorentz-Lorenz expression
$$
\mathrm{MR}=\frac{n_{0}^{2}-1}{n_{0}^{2}+2} \frac{\mathrm{MW}}{d}
$$

MR is of interest because of its relationship to molecular polarizability. ${ }^{3,30,35,36}$ Values of the properties employed for the $74 \mathrm{C}_{2}-\mathrm{C}_{9}$ alkanes are shown in Table I. Only liquid-phase values for MV, MR, HV, and ST were used. The extremely hindered compound $2,2,3,3$-tetramethylbutane (39) is a solid at $25^{\circ} \mathrm{C}$; its $\mathrm{mp}\left(+100.7^{\circ} \mathrm{C}\right)$ was judged to be an outlier. Compounds $1-4$ are gases at $20^{\circ} \mathrm{C}$ and 1 atm .

Parameters. Four decades ago Wiener introduced an index based on path distances. ${ }^{16,17}$ The Wiener index $w$ is the sum of all unique, shortest path distances, in terms of $\mathrm{C}-\mathrm{C}$ bonds, in the carbon skeleton ("hydrogen-suppressed graph") of the hydrocarbon. For example, for 2-methylbutane

$$
\mathrm{C}_{1}-{\stackrel{C}{C_{2}}}_{\mathrm{C}_{5}-\mathrm{C}_{3}-\mathrm{C}_{4}}
$$

the Wiener index is obtained as half the sum of the elements in the distance matrix $\mathbf{D}$

$$
\mathbf{D}=\left(\begin{array}{lllll}
0 & 1 & 2 & 3 & 2 \\
1 & 0 & 1 & 2 & 1 \\
2 & 1 & 0 & 1 & 2 \\
3 & 2 & 1 & 0 & 3 \\
2 & 1 & 2 & 3 & 0
\end{array}\right)
$$

i.e., $w=18$. (In the distance matrix each unique path is included twice, as $d_{i j}$ and as $d_{j i}$.) The Wiener index increases with the number of carbon atoms; it is lower for branched isomers than for more extended isomers. In many applications the reduced Wiener index, $w_{\mathrm{r}}=w / N_{\mathrm{c}}{ }^{2}$, is used, where $N_{\mathrm{c}}$ is the number of carbon atoms. ${ }^{15}$ Wiener also introduced the parameter $p_{3}$, the number of unique paths of length $3 \mathrm{C}-\mathrm{C}$ bonds, originally as a "polarizability" factor ${ }^{16,17}$ but later associated with steric crowding. ${ }^{19}$ As seen from either the carbon skeleton or the distance matrix, for 2 -methylbutane, $p_{3}=2$. In some cases a modified Wiener index, $w_{\text {mod }}=w+p_{3}$, has been used. Platt ${ }^{19}$ introduced the parameter $f$, calculated by taking the number of adjacent bonds to each bond and summing these values for all bonds in the carbon skeleton. For $2-$ methylbutane $f=2\left(\mathrm{C}_{1}-\mathrm{C}_{2}\right)+3\left(\mathrm{C}_{2}-\mathrm{C}_{3}\right)+1\left(\mathrm{C}_{3}-\mathrm{C}_{4}\right)+2\left(\mathrm{C}_{2}-\mathrm{C}_{5}\right)=8$. The inverses of $w$ and $w_{r}$ were also included in this parameter set.

Randic introduced the concept of a connectivity (branching) index in 1975. ${ }^{20}$ The concept has been further developed and applied extensively by Randić, Kier, Hall, and their coworkers. ${ }^{9,14}$ Each carbon atom $i$ in the carbon skeleton of a hydrocarbon is assigned a valence. $\delta_{1}$, equal to the number of carbon bonds to that atom. The zeroth-order connectivity index ${ }^{0} \chi$ is then the sum over all atoms 1 (eq 1). For 2-methylbutane

$$
\begin{equation*}
{ }^{0} \chi=\sum_{\text {atoms }} 1 / \delta_{i}^{1 / 2} \tag{1}
\end{equation*}
$$

${ }^{0} \chi=1 / \sqrt{1}+1 / \sqrt{3}+1 / \sqrt{2}+1 / \sqrt{1}+1 / \sqrt{1}=4.284$. The first-order connectivity index ${ }^{1} \chi$ is the sum over all bonds $i-j$ (eq 2). For

$$
\begin{equation*}
{ }^{1} \chi=\sum_{\text {bonds }} 1 /\left(\delta_{i} \delta_{j}\right)^{1 / 2} \tag{2}
\end{equation*}
$$

2-methylbutane ${ }^{1} \chi=1 / \sqrt{2}+1 / \sqrt{6}+1 / \sqrt{2}+1 / \sqrt{3}=2.400$. The second-order index ${ }^{2} \chi$ is a sum over 2 -bond paths $i-j-k$ of terms $1 /$ $\left(\delta_{i} \delta_{j} \delta_{k}\right)^{1 / 2}$. A hierarchy of additional indices ${ }^{m} \chi_{t}$ of order $m$ and type $t$ can be obtained by summing analogous terms over substructural units involving paths ( $t=p$ ), clusters ( $t=c$ ), or path-cluster ( $t=p c$ ) combinations of $m$ bonds. Values for these indices for the 74 alkanes were

[^2]taken from Appendix I of Kier and Hall's book. ${ }^{9}$ The total structure index $x_{1}$ can be calculated with all the carbon valences of the compound (eq 3). The above indices, plus the inverses of ${ }^{0} \chi,{ }^{1} \chi$, and $\chi_{t}$, were used in this parameter set.
\[

$$
\begin{equation*}
\chi_{\mathrm{t}}=1 /\left(\delta_{1} \cdot \delta_{2} \cdots \delta_{m}\right)^{1 / 2} \tag{3}
\end{equation*}
$$

\]

Information indices have been used successfully in a variety of applications in chemistry. ${ }^{12,21}$ Several different types of information indices can be defined. ${ }^{12,38}$ When Kier's approach ${ }^{39}$ is followed, the atoms of a compound are divided into classes according to their equivalence or nonequivalence. In 2 -methylbutane, carbons 1 and 5 are equivalent and the remaining carbons are unique; therefore, there are four classes of carbon atoms, one containing two members and three containing one member each. Likewise, there are four classes of hydrogen atoms containing six, one, two, and three members, respectively. Following from Shannon's information theorem, Kier's information index ("molecular negentropy") $I$ is defined as ${ }^{39}$ in eq 4 where $p_{i}=n_{t} / N$ is the probability

$$
\begin{align*}
I & =-N \sum p_{i} \log p_{i} \\
& =N \log N-\sum n_{1} \log n_{i} \tag{4}
\end{align*}
$$

of class $i, n_{i}$ is the number of members in class $i$, and $N$ is the total number of atoms in the compound. If only carbon atoms are considered, one obtains the index ICM. Basak ${ }^{21}$ has defined additional indices, as

$$
\begin{equation*}
\mathrm{IC}=I / N \tag{5}
\end{equation*}
$$

$\mathrm{SIC}=\mathrm{IC} / \log N$
$\mathrm{CIC}=(1 / N) \sum n_{i} \log n_{i}$
The indices I, ICM, IC, SIC, and CIC together formed the information index parameter set.

In some recent studies specific ad hoc indices have been shown to give a good account of several properties. ${ }^{15,22.40}$ The simplest representative of molecular mass or volume is $N_{\mathrm{c}}$, the number of carbon atoms. Because each branch of a hydrocarbon terminates as a methyl group, the number of terminal methyl groups, $T_{\mathrm{m}}$, is a crude measure of branching. Randic̃ first suggested the use of $T_{3}$, the number of terminal methyls separated by 3 bonds, as a steric parameter in analysis of chromatographic retention data. ${ }^{41}$ The steric index $p_{3}$ has been identified above in connection with the Wiener scheme. The inverse $1 / N_{c}$ and the quadratic terms $N_{c}{ }^{2}, T_{3}{ }^{2}$, and $T_{\mathrm{m}}{ }^{2}$ were also included in this parameter set.

Molecular volumes $V_{\mathrm{B}}$ and surface areas $A_{\mathrm{B}}$ were calculated from sums of contributions as described by Bondi. ${ }^{23}$ Values for the most significant parameters described above for the 74 alkanes are given in Table II.

Regression equations and other statistical measures were obtained by options in the SAS software package ${ }^{42}$ on an IBM 8083E computer.

Factor Analysis. Factor analysis ${ }^{43-46}$ is a multivariate statistical technique for estimating the inherent dimensionality of a set of variables. It rests on the assumption that the experimental variables of interest can be considered to depend on a (presumably smaller) set of hypothetical underlying variables or factors. Observed correlations among the experimental variables are assumed to result from their common dependences on these underlying factors.

In principal component analysis (PCA) a matrix is first constructed consisting of the correlations (or covariances) among the variables of interest. The eigenvalues and eigenvectors of this matrix are then determined. The eigenvectors so obtained are orthogonal, and the sum of their eigenvalues equals the original number of variables. Each eigenvector is a linear combination of the original variables and represents a principal component, or initial factor. The coefficient of an observed variable in a factor is termed the loading of that variable on the factor. The relative importance of each factor is related to the magnitude of its eigenvalue. The process can be viewed as one in which the first principal component axis is constructed to account for a maximum amount of variance in the data; the second component axis accounts for a maximum amount of the remaining variance under the constraint that it be or-

[^3]Table I. Experimental Values for the Physical Properties of the 74 Alkanes

| observn | name | bp | MV | MR | HV | TC | PC | ST | mp |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2 | -88.630 |  |  |  | 32.27 | 48.20 |  | -183.27 |
| 2 | 3 | -42.070 |  |  |  | 96.80 | 42.01 |  | -187.69 |
| 3 | 4 | -0.500 |  |  |  | 152.01 | 37.47 |  | -138.35 |
| 4 | 2M3 | -11.730 |  |  |  | 134.98 | 36.00 |  | -159.60 |
| 5 | 5 | 36.074 | 115.205 | 25.2656 | 26.42 | 196.62 | 33.31 | 16.00 | -129.72 |
| 6 | 2M4 | 27.852 | 116.426 | 25.2923 | 24.59 | 187.80 | 32.90 | 15.00 | -159.90 |
| 7 | 22MM3 | 9.503 | 122.074 | 25.7243 | 21.78 | 160.60 | 31.57 |  | -16.55 |
| 8 | 6 | 68.740 | 130.688 | 29.9066 | 31.55 | 234.70 | 29.92 | 18.42 | -95.35 |
| 9 | 2M5 | 60.271 | 131.933 | 29.9459 | 29.86 | 224.90 | 29.95 | 17.38 | -153.67 |
| 10 | 3M5 | 63.282 | 129.717 | 29.8016 | 30.27 | 231.20 | 30.83 | 18.12 | -118.00 |
| 11 | 22MM4 | 49.741 | 132.744 | 29.9347 | 27.69 | 216.20 | 30.67 | 16.30 | -99.87 |
| 12 | 23MM4 | 57.988 | 130.240 | 29.8104 | 29.12 | 227.10 | 30.99 | 17.37 | -128.54 |
| 13 | 7 | 98.427 | 146.540 | 34.5504 | 36.55 | 267.01 | 27.01 | 20.26 | -90.61 |
| 14 | 2M6 | 90.052 | 147.656 | 34.5908 | 34.80 | 257.90 | 27.20 | 19.29 | -118.28 |
| 15 | 3M6 | 91.850 | 145.821 | 34.4597 | 35.08 | 262.40 | 28.10 | 19.79 | -119.40 |
| 16 | 3E5 | 93.475 | 143.517 | 34.2827 | 35.22 | 267.60 | 28.60 | 20.44 | -118.60 |
| 17 | 22MM5 | 79.197 | 148.695 | 34.6166 | 32.43 | 247.70 | 28.40 | 18.02 | -123.81 |
| 18 | 23MM5 | 89.784 | 144.153 | 34.3237 | 34.24 | 264.60 | 29.20 | 19.96 | -119.10 |
| 19 | 24MM5 | 80.500 | 148.949 | 34.6192 | 32.88 | 247.10 | 27.40 | 18.15 | -119.24 |
| 20 | 33MM5 | 86.064 | 144.530 | 34.3323 | 33.02 | 263.00 | 30.00 | 19.59 | -134.46 |
| 21 | 223MMM4 | 80.882 | 145.191 | 34.3736 | 32.04 | 258.30 | 29.75 | 18.76 | -24.91 |
| 22 | 8 | 125.665 | 162.592 | 39.1922 | 41.48 | 296.20 | 24.64 | 21.76 | -56.79 |
| 23 | 2M7 | 117.647 | 163.663 | 39.2316 | 39.68 | 288.00 | 24.80 | 20.60 | -109.04 |
| 24 | 3M7 | 118.925 | 161.832 | 39.1001 | 39.83 | 292.00 | 25.60 | 21.17 | -120.50 |
| 25 | 4M7 | 117.709 | 162.105 | 39.1174 | 39.67 | 290.00 | 25.60 | 21.00 | -120.95 |
| 26 | 3E6 | 118.534 | 160.072 | 38.9441 | 39.40 | 292.00 | 25.74 | 21.51 |  |
| 27 | 22MM6 | 106.840 | 164.285 | 39.2525 | 37.29 | 279.00 | 25.60 | 19.60 | -121.18 |
| 28 | 23MM6 | 115.607 | 160.395 | 38.9808 | 38.79 | 293.00 | 26.60 | 20.99 |  |
| 29 | 24MM6 | 109.429 | 163.093 | 39.1300 | 37.76 | 282.00 | 25.80 | 20.05 | -137.50 |
| 30 | 25MM6 | 109.103 | 164.697 | 39.2596 | 37.86 | 279.00 | 25.00 | 19.73 | -91.20 |
| 31 | 33MM6 | 111.969 | 160.879 | 39.0087 | 37.93 | 290.84 | 27.20 | 20.63 | -126.10 |
| 32 | 34MM6 | 117.725 | 158.814 | 38.8453 | 39.02 | 298.00 | 27.40 | 21.64 |  |
| 33 | 23ME5 | 115.650 | 158.794 | 38.8362 | 38.52 | 295.00 | 27.40 | 21.52 | -114.96 |
| 34 | 33ME5 | 118.259 | 157.026 | 38.7171 | 37.99 | 305.00 | 28.90 | 21.99 | -90.87 |
| 35 | $223 \mathrm{MMM5}$ | 109.841 | 159.526 | 38.9249 | 36.91 | 294.00 | 28.20 | 20.67 | -112.27 |
| 36 | 224MMM5 | 99.238 | 165.083 | 39.2617 | 35.13 | 271.15 | 25.50 | 18.77 | -107.38 |
| 37 | 233MMM5 | 114.760 | 157.292 | 38.7617 | 37.22 | 303.00 | 29.00 | 21.56 | -100.70 |
| 38 | 234MMM5 | 113.467 | 158.852 | 38.8681 | 37.61 | 295.00 | 27.60 | 21.14 | -109.21 |
| 39 | 2233MMMM4 | 106.470 |  |  |  | 270.80 | 24.50 |  |  |
| 40 | $9$ | 150.798 | 178.713 | 43.8423 | 46.44 | 322.00 | 22.74 | 22.92 | -53.52 |
| 41 | 2M8 | 143.260 | 179.773 | 43.8795 | 44.65 | 315.00 | 23.60 | 21.88 | -80.40 |
| 42 | 3M8 | 144.180 | 177.952 | 43.7296 | 44.75 | 318.00 | 23.70 | 22.34 | -107.60 |
| 43 | 4M8 | 142.480 | 178.150 | 43.7687 | 44.75 | 318.30 | 23.06 | 22.34 | -113.20 |
| 44 | 3E7 | 143.000 | 176.410 | 43.6420 | 44.81 | 318.00 | 23.98 | 22.81 | -114.90 |
| 45 | 4E7 | 141.200 | 175.685 | 43.4907 | 44.81 | 318.30 | 23.98 | 22.81 |  |
| 46 | 22MM7 | 132.690 | 180.507 | 43.9138 | 42.28 | 302.00 | 22.80 | 20.80 | -113.00 |
| 47 | 23MM7 | 140.500 | 176.653 | 43.6269 | 43.79 | 315.00 | 23.79 | 22.34 | -116.00 |
| 48 | 24MM7 | 133.500 | 179.120 | 43.7393 | 42.87 | 306.00 | 22.70 | 21.30 |  |
| 49 | 25 MM 7 | 136.000 | 179.371 | 43.8484 | 42.87 | 307.80 | 22.70 | 21.30 |  |
| 50 | 26MM7 | 135.210 | 180.914 | 43.9258 | 42.82 | 306.00 | 23.70 | 20.83 | -102.90 |
| 51 | 33MM7 | 137.300 | 176.897 | 43.6870 | 42.66 | 314.00 | 24.19 | 22.01 |  |
| 52 | 34 MM 7 | 140.600 | 175.349 | 43.5473 | 43.84 | 322.70 | 24.77 | 22.80 |  |
| 53 | 35MM7 | 136.000 | 177.386 | 43.6378 | 42.98 | 312.30 | 23.59 | 21.77 |  |
| 54 | 44MM7 | 135.200 | 176.897 | 43.6022 | 42.66 | 317.80 | 24.18 | 22.01 |  |
| 55 | 23ME6 | 138.000 | 175.445 | 43.6550 | 43.84 | 322.70 | 24.77 | 22.80 |  |
| 56 | 24ME6 | 133.800 | 177.386 | 43.6472 | 42.98 | 330.3 | 25.56 | 21.77 |  |
| 57 | 33ME6 | 140.600 | 173.077 | 43.2680 | 43.04 | 327.2 | 25.66 | 23.22 |  |
| 58 | 34ME6 | 140.400 | 172.844 | 43.3746 | 43.95 | 312.3 | 23.59 | 23.27 |  |
| 59 | 123MMM6 | 133.600 | 175.878 | 43.6226 | 41.91 | 318.1 | 25.07 | 21.86 |  |
| 60 | 224MMM6 | 126.540 | 179.220 | 43.7638 | 40.57 | 301.0 | 23.39 | 20.51 | -120.00 |
| 61 | 225MMM6 | 124.084 | 181.346 | 43.9356 | 40.17 | 296.6 | 22.41 | 20.04 | -105.78 |
| 62 | 233MMM6 | 137.680 | 173.780 | 43.4347 | 42.23 | 326.1 | 25.56 | 22.41 | -116.80 |
| 63 | 234MMM6 | 139.000 | 173.498 | 43.3917 | 42.93 | 324.2 | 25.46 | 22.80 |  |
| 64 | 235MMM6 | 131.340 | 177.656 | 43.6474 | 41.42 | 309.4 | 23.49 | 21.27 | -127.80 |
| 65 | 244MMM6 | 130.648 | 177.187 | 43.6598 | 40.84 | 309.1 | 23.79 | 21.17 | -113.38 |
| 66 | 334MMM6 | 140.460 | 172.055 | 43.3407 | 42.28 | 330.6 | 26.45 | 23.27 | -101.20 |
| 67 | 33EE5 | 146.168 | 170.185 | 43.1134 | 43.36 | 342.8 | 26.94 | 23.75 | -33.11 |
| 68 | 223MME5 | 133.830 | 174.537 | 43.4571 | 42.02 | 322.6 | 25.96 | 22.38 | -99.20 |
| 69 | 233MME5 | 142.000 | 170.093 | 42.9542 | 42.55 | 338.6 | 26.94 | 23.87 |  |
| 70 | 234MEM5 | 136.730 | 173.804 | 43.4037 | 42.93 | 324.2 | 25.46 | 22.80 | -122.20 |
| 71 | 2233(M) 5 | 140.274 | 169.495 | 43.2147 | 41.00 | 334.5 | 27.04 | 23.38 | -9.90 |
| 72 | 2234(M) 5 | 133.016 | 173.557 | 43.4359 | 41.00 | 319.6 | 25.66 | 21.98 | -121.09 |
| 73 | 2244(M) 5 | 122.284 | 178.256 | 43.8747 | 38.10 | 301.6 | 24.58 | 20.37 | -66.54 |
| 74 | 2334(M)5 | 141.551 | 169.928 | 43.2016 | 41.75 | 334.5 | 26.85 | 23.31 | -102.12 |

[^4] as in Kier and Hall: ${ }^{9} 2=$ ethane, $3=$ propane, etc.; $M=$ methyl, $E=$ ethyl; e.g., $34 \mathrm{ME} 6=3$-methyl-4-ethylhexane

Table II. Selected Parameter Values for the 74 Alkanes

| observn | name | $W$ | $p_{3}$ | $f$ | ${ }^{0} \chi$ | ${ }^{1} \chi$ | $\chi_{\text {t }}$ | $N_{\text {c }}$ | $T_{m}$ | $T_{3}$ | I |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2 | 1 | 0 | 0 | 2.00000 | 1.00000 | 1.0000 | 2 | 2 | 0 | 1.9538 |
| 2 | 3 | 4 | 0 | 2 | 2.70710 | 1.41421 | 0.7071 | 3 | 2 | 0 | 5.5823 |
| 3 | 4 | 10 | 1 | 4 | 3.41421 | 1.91421 | 0.5000 | 4 | 2 | 1 | 7.7645 |
| 4 | 2 M 3 | 9 | 0 | 6 | 3.57735 | 1.73205 | 0.5774 | 4 | 3 | 0 | 6.0262 |
| 5 | 5 | 20 | 2 | 6 | 4.12132 | 2.41421 | 0.3536 | 5 | 2 | 0 | 12.0343 |
| 6 | 2 M 4 | 18 | 2 | 8 | 4.28445 | 2.27005 | 0.4082 | 5 | 3 | 2 | 13.6132 |
| 7 | 22MM3 | 16 | 0 | 12 | 4.50000 | 2.00000 | 0.5000 | 5 | 4 | 0 | 5.5592 |
| 8 | 6 | 35 | 3 | 8 | 4.82842 | 2.91421 | 0.2500 | 6 | 2 | 0 | 14.7290 |
| 9 | 2M5 | 32 | 3 | 10 | 4.99156 | 2.77005 | 0.2887 | 6 | 3 | 0 | 18.1141 |
| 10 | 3 M 5 | 31 | 4 | 10 | 4.99156 | 2.80806 | 0.2887 | 6 | 3 | 2 | 16.3080 |
| 11 | 22MM4 | 28 | 3 | 14 | 5.20710 | 2.56066 | 0.3536 | 6 | 4 | 3 | 13.9676 |
| 12 | 23MM4 | 29 | 4 | 12 | 5.15470 | 2.64273 | 0.3333 | 6 | 4 | 4 | 9.4581 |
| 13 | 7 | 56 | 4 | 10 | 5.53553 | 3.41421 | 0.1768 | 7 | 2 | 0 | 19.4261 |
| 14 | 2 M 6 | 52 | 4 | 12 | 5.69867 | 3.27005 | 0.2041 | 7 | 3 | 0 | 22.8112 |
| 15 | 3 M 6 | 50 | 5 | 12 | 5.69867 | 3.30806 | 0.2041 | 7 | 3 | 1 | 25.2195 |
| 16 | 3E5 | 48 | 6 | 12 | 5.69867 | 3.34606 | 0.2041 | 7 | 3 | 0 | 15.1999 |
| 17 | 22MM5 | 46 | 4 | 16 | 5.91421 | 3.06066 | 0.2500 | 7 | 4 | 0 | 18.6647 |
| 18 | 23MM5 | 46 | 6 | 14 | 5.86180 | 3.18073 | 0.2357 | 7 | 4 | 3 | 22.5840 |
| 19 | 24MM5 | 48 | 4 | 14 | 5.86180 | 3.12589 | 0.2357 | 7 | 4 | 0 | 14.1551 |
| 20 | 33MM5 | 44 | 6 | 16 | 5.91421 | 3.12132 | 0.2500 | 7 | 4 | 4 | 17.7675 |
| 21 | 223MMM4 | 42 | 6 | 18 | 6.07735 | 2.94337 | 0.2887 | 7 | 5 | 6 | 16.0292 |
| 22 | 8 | 84 | 5 | 12 | 6.24264 | 3.91421 | 0.1250 | 8 | 2 | 0 | 22.4874 |
| 23 | 2M7 | 79 | 5 | 14 | 6.40577 | 3.77005 | 0.1443 | 8 | 3 | 0 | 27.6787 |
| 24 | 3 M 7 | 76 | 6 | 14 | 6.40577 | 3.80806 | 0.1443 | 8 | 3 | 1 | 30.0870 |
| 25 | 4M7 | 75 | 6 | 14 | 6.40577 | 3.80806 | 0.1443 | 8 | 3 | 0 | 24.0664 |
| 26 | 3E6 | 72 | 7 | 14 | 6.40577 | 3.84606 | 0.1443 | 8 | 3 | 0 | 25.8726 |
| 27 | 22MM6 | 71 | 5 | 18 | 6.62132 | 3.56066 | 0.1768 | 8 | 4 | 0 | 23.5322 |
| 28 | 23MM6 | 70 | 7 | 16 | 6.56891 | 3.68073 | 0.1667 | 8 | 4 | 2 | 27.4515 |
| 29 | 24MM6 | 71 | 6 | 16 | 6.56891 | 3.66390 | 0.1667 | 8 | 4 | 1 | 27.4515 |
| 30 | 25MM6 | 74 | 5 | 16 | 6.56891 | 3.62589 | 0.1667 | 8 | 4 | 0 | 17.2165 |
| 31 | 33MM6 | 67 | 7 | 18 | 6.62132 | 3.62132 | 0.1768 | 8 | 4 | 2 | 26.8494 |
| 32 | 34MM6 | 68 | 8 | 16 | 6.56891 | 3.71874 | 0.1667 | 8 | 4 | 3 | 22.0330 |
| 33 | 23ME5 | 67 | 8 | 16 | 6.56891 | 3.71874 | 0.1667 | 8 | 4 | 0 | 23.2371 |
| 34 | 33ME5 | 64 | 9 | 18 | 6.62132 | 3.68198 | 0.1768 | 8 | 4 | 3 | 19.2381 |
| 35 | 223MMM5 | 63 | 8 | 20 | 6.78445 | 3.48138 | 0.2041 | 8 | 5 | 4 | 23.3050 |
| 36 | 224MMM5 | 66 | 5 | 20 | 6.78445 | 3.41650 | 0.2041 | 8 | 5 | 0 | 20.8967 |
| 37 | 233MMM5 | 62 | 9 | 20 | 6.78445 | 3.50403 | 0.2041 | 8 | 5 | 6 | 24.2139 |
| 38 | 234 MMM5 | 65 | 8 | 18 | 6.73205 | 3.55341 | 0.1925 | 8 | 5 | 4 | 18.7954 |
| 39 | 2233MMMM4 | 58 | 9 | 24 | 7.00000 | 3.25000 | 0.2500 | 8 | 6 | 9 | 8.9234 |
| 40 | 9 | 120 | 6 | 14 | 6.94974 | 4.41421 | 0.0884 | 9 | 2 | 0 | 27.5056 |
| 41 | 2M8 | 114 | 6 | 16 | 7.11288 | 4.27005 | 0.1021 | 9 | 3 | 0 | 32.6969 |
| 42 | 3 M 8 | 110 | 7 | 16 | 7.11288 | 4.30806 | 0.1021 | 9 | 3 | 1 | 35.1052 |
| 43 | 4M8 | 108 | 7 | 16 | 7.11288 | 4.30806 | 0.1021 | 9 | 3 | 0 | 35.1052 |
| 44 | 3E7 | 104 | 8 | 16 | 7.11288 | 4.34606 | 0.1021 | 9 | 3 | 0 | 30.8907 |
| 45 | 4E7 | 102 | 8 | 16 | 7.11288 | 4.34606 | 0.1021 | 9 | 3 | 0 | 29.0846 |
| 46 | 22MM7 | 104 | 6 | 20 | 7.32842 | 4.06066 | 0.1250 | 9 | 4 | 0 | 28.5504 |
| 47 | 23MM7 | 102 | 8 | 18 | 7.27602 | 4.18073 | 0.1179 | 9 | 4 | 2 | 32.4697 |
| 48 | 24MM7 | 102 | 7 | 18 | 7.27602 | 4.16390 | 0.1179 | 9 | 4 | 0 | 32.4697 |
| 49 | 25MM7 | 104 | 7 | 18 | 7.27602 | 4.16390 | 0.1179 | 9 | 4 | 1 | 32.4697 |
| 50 | 26MM7 | 108 | 6 | 18 | 7.27602 | 4.12589 | 0.1179 | 9 | 4 | 0 | 22.2346 |
| 51 | 33MM7 | 98 | 8 | 20 | 7.32842 | 4.12132 | 0.1250 | 9 | 4 | 2 | 31.8676 |
| 52 | 34MM7 | 98 | 9 | 18 | 7.27602 | 4.21874 | 0.1179 | 9 | 4 | 2 | 34.8779 |
| 53 | 35MM7 | 100 | 8 | 18 | 7.27602 | 4.20190 | 0.1179 | 9 | 4 | 2 | 27.0511 |
| 54 | 44MM7 | 96 | 8 | 20 | 7.32842 | 4.12132 | 0.1250 | 9 | 4 | 0 | 25.8470 |
| 55 | 23ME6 | 96 | 9 | 18 | 7.27602 | 4.21874 | 0.1179 | 9 | 4 | 0 | 32.4697 |
| 56 | 24ME6 | 98 | 8 | 18 | 7.27602 | 4.20190 | 0.1179 | 9 | 4 | 0 | 28.2552 |
| 57 | 33ME6 | 92 | 10 | 20 | 7.32842 | 4.18198 | 0.1250 | 9 | 4 | 2 | 30.0614 |
| 58 | 34ME6 | 94 | 10 | 18 | 7.27602 | 4.25674 | 0.1179 | 9 | 4 | 1 | 30.6635 |
| 59 | 223MMM6 | 92 | 9 | 22 | 7.49156 | 3.98138 | 0.1443 | 9 | 5 | 3 | 28.3231 |
| 60 | 224MMM6 | 94 | 7 | 22 | 7.49156 | 3.95450 | 0.1443 | 9 | 5 | 1 | 28.3231 |
| 61 | 225MMM6 | 98 | 6 | 22 | 7.49156 | 3.91650 | 0.1443 | 9 | 5 | 0 | 25.9149 |
| 62 | 233MMM6 | 90 | 10 | 22 | 7.49156 | 4.00403 | 0.1443 | 9 | 5 | 4 | 29.2321 |
| 63 | 234MMM6 | 92 | 10 | 20 | 7.43915 | 4.09142 | 0.1361 | 9 | 5 | 4 | 32.2424 |
| 64 | 235MMM6 | 96 | 8 | 20 | 7.43915 | 4.03658 | 0.1361 | 9 | 5 | 2 | 29.8342 |
| 65 | 244MMM6 | 92 | 8 | 22 | 7.49156 | 3.97716 | 0.1443 | 9 | 5 | 2 | 29.2321 |
| 66 | 334MMM6 | 88 | 11 | 22 | 7.49156 | 4.04204 | 0.1443 | 9 | 5 | 5 | 31.6404 |
| 67 | 33EE5 | 88 | 12 | 20 | 7.32842 | 4.24264 | 0.1250 | 9 | 4 | 0 | 17.4182 |
| 68 | 223MME5 | 88 | 10 | 22 | 7.49156 | 4.01938 | 0.1443 | 9 | 5 | 0 | 24.1087 |
| 69 | 233MME5 | 86 | 12 | 22 | 7.49156 | 4.06469 | 0.1443 | 9 | 5 | 4 | 27.4259 |
| 70 | 234MEM5 | 90 | 10 | 20 | 7.43915 | 4.09142 | 0.1361 | 9 | 5 | 0 | 23.8136 |
| 71 | 2233MMMM | 82 | 12 | 26 | 7.70710 | 3.81066 | 0.1768 | 9 | 6 | 8 | 25.0856 |
| 72 | 2234 MMMM | 86 | 10 | 24 | 7.65470 | 3.85405 | 0.1667 | 9 | 6 | 5 | 25.6877 |
| 73 | 2244MMMM | 88 | 6 | 26 | 7.70710 | 3.70710 | 0.1768 | 9 | 6 | 0 | 13.9416 |
| 74 | 2334MMMM | 84 | 12 | 24 | 7.65470 | 3.88675 | 0.1667 | 9 | 6 | 8 | 20.5760 |

thogonal to the first component, and so forth, until all component axes are constructed. For every object in the data set a numerical value for
each factor can be obtained from the values of the variables; these numerical values are termed factor scores. PCA has previously been applied

Table III. Correlations among the Physical Properties Examined

|  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | bp | MV | MR | HV | TC | PC | ST |
| bp | 1.000 |  |  |  |  |  |  |
| MV | 0.948 | 1.000 |  |  |  |  |  |
| MR | 0.972 | 0.992 | 1.000 |  |  |  |  |
| HV | 0.989 | 0.942 | 0.957 | 1.000 |  |  |  |
| TC | 0.993 | 0.911 | 0.952 | 0.955 | 1.000 | 1.000 |  |
| PC | -0.932 | -0.931 | -0.892 | -0.875 | -0.898 |  |  |
| ST | 0.946 | 0.807 | 0.865 | 0.922 | 0.965 | -0.650 | 1.000 |
| mp | 0.457 | 0.143 | 0.157 | 0.122 | 0.472 | -0.436 | 0.421 |

to liquid-state properties, ${ }^{47-49}$ structural descriptors, ${ }^{50}$ and other chemical problems. ${ }^{51,52}$

The question of how many components are significant in such an analysis is not simply answered. In the social sciences a common guide has been to retain only components with eigenvalues greater than unity, but this requirement is surely too stringent for the more accurate physical data analyzed here; in general, it is deemed wisest to use several criteria to assist in making this decision. ${ }^{44}$ Possible criteria include a lower acceptable magnitude for the retained eigenvalues (based on the perceived accuracy of the data), the scree-test, and Kaiser's measure of sampling adequacy, MSA. ${ }^{44,46}$ Despite these aids, any decision on this question remains somewhat subjective.

Principal component analysis does not necessarily lead to the most physically meaningful or readily interpretable factorization. First, it is often possible, with rather standard statistical criteria, to achieve a "simpler" factor structure by performing orthogonal rotations on the initial factors. This arises because neither the factors nor their loadings are uniquely defined. Second, in the present example there is no a priori physical reason to require that the factors be orthogonal; oblique rotations can be expected in some cases to yield more reasonable representations of the factor structure. Subsequent rotations do not, however, change the number of factors or the total fraction of variance accounted for by the factors.

Factor analysis, including PCA and orthogonal and oblique rotations, was performed with the VARIMAX and PROMAX options within PROC FACTOR of the SAS software package. ${ }^{42.46}$

## Results

Before other analyses of the data are attempted, it is instructive to examine the correlations among the physical properties for the 74 alkanes, as shown in Table III. It is readily apparent that strong internal correlations are present among most of the properties. Melting points are an exception, being only weakly correlated with the other properties. Surface tension is another possible exception. For the remaining six properties all the correlation coefficients $(r)$ are greater than 0.875 , and for the subset (bp, MV, MR, HV), all correlations exceed 0.942. It may be anticipated, then, that the factor analysis should reveal some lower (than eight) number of inherent dimensions for these physical properties. Furthermore, it can be anticipated that if a given set of structural parameters successfully models a given property, this parameter set should also be reasonably successful in modeling other, strongly correlated properties. The converse can also be anticipated; i.e., lack of success should transfer to correlated properties.

Regression Equations. Table IV shows coefficients of determination $\left(r^{2}\right)$ and standard errors $(s)$ for the most successful one-, two-, and three-parameter models of the eight physical properties. (Note that $r^{2}$ gives the fraction of the variance in the data that is accounted for by the model.) Overall, the most successful single parameters are seen to be the connectivity indices ${ }^{1} \chi$ and ${ }^{0} \chi$, the number of carbons $N_{\mathrm{c}}$, and the calculated (Bondi) volume $V_{\mathrm{B}}$. Correlations among these parameters and some other selected

[^5]

Figure 1. Principal components $f 1$ and $f 2$ for the eight physical properties.
indices are shown in Table $V$. It is apparent that the leading single parameters are themselves intercorrelated and related to molecular volume.

Whereas the connectivity indices and ad hoc descriptors typically are superior to the Wiener and information indices at the single-term level, it is evident from Table IV that the latter parameter sets tend to "catch up" as additional terms are included. At the three-term level the four approaches tend toward a degree of similarity among their multiple correlation coefficients. On the basis of the standard errors $s$-which are more sensitive measures than $r^{2}$-overall, the connectivity indices and ad hoc descriptors are superior to the other indices in fitting the data for the present set of alkane properties.

Most of the physical properties are reasonably well accounted for by the present parameters even at the three-term level. The melting points ( mp ) are a notable exception, being not well modeled by any of the parameter sets. Surface tensions (ST) and critical pressures (PC) are less well accounted for generally than the remaining physical properties. As a rule, the fits of the properties at the three-term level fall in the same relative order as those from the single-term $V_{\mathrm{B}}$ and $A_{\mathrm{B}}$ models.

More exact regression equations for the eight physical properties are shown in Table VI for the connectivity indices and in Table VII for the ad hoc descriptors. With an aim of simplicity, these equations have been arbitrarily limited to no more than five parameters. Fewer parameters were included when $F$-statistics indicated that additional parameters were not significant. The ad hoc descriptors are as a rule more easily calculated and interpreted physically and thus may be more useful for some applications. For purposes of interpretation, the equations of Table VII have been dissected into mass ( $N_{\mathrm{c}}, N_{\mathrm{c}}{ }^{2}, 1 / N_{\mathrm{c}}$ ), branching ( $T_{m}$ ), and steric ( $T_{3}, p_{3}$ ) contributions by multiplying the coefficients by the mean parameter values; fractional contributions were obtained by multiplying the absolute values by the coefficient of determination $\left(r^{2}\right)$ and dividing by the sum. The results are shown in Table VIII. It is clear that molecular mass makes a dominant contribution for most properties, with smaller influences from branching and steric factors.

Factor Analysis. Results of the principal component analysis are shown in Table IX. In the analysis for all 8 properties and 51 compounds the first factor (fl) dominates and accounts for

Table IV. Summary of Results for One-, Two-, and Three-Parameter Models for the Eight Physical Properties

| property | Wiener indices |  |  |  | connectivity indices |  |  |  |  | information indices |  |  |  |  | ad hoc descriptors |  |  |  |  | volume/area |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | param |  | $r^{2}$ | $s$ | param |  |  | $r^{2}$ | $s$ | param |  |  | $r^{2}$ | $s$ | param |  |  | $r^{2}$ | $s$ | param | $r^{2}$ | $s$ |
| $\mathrm{bp}\left({ }^{\circ} \mathrm{C}\right)$ | $w_{\text {mod }}$ |  | 0.86 | 17.0 | ${ }^{1} \chi$ |  |  | 0.969 | 8.3 | I |  |  | 0.701 | 25.5 | $N_{\text {c }}$ |  |  | 0.971 | 7.9 | vol | 0.971 | 7.9 |
| $n=74$ | $w_{\text {r }}$ | $p_{3}$ | 0.982 | 6.3 | ${ }^{1} \chi$ | $1 /{ }^{0} \chi$ |  | 0.991 | 4.4 | 1 | CIC |  | 0.930 | 12.5 | $N_{\text {c }}$ | $N_{c}{ }^{2}$ |  | 0.982 | 6.4 | area | 0.962 | 9.1 |
|  | $w_{\text {r }}$ | $p_{3} 1 / w_{\text {r }}$ | 0.995 | 3.4 | ${ }^{1} \chi$ | $\chi_{1}$ | ${ }^{4} \chi_{\text {pc }}$ | 0.998 | 2.1 | I | CIC | SIC | 0.983 | 6.3 | $N_{\text {c }}$ | $N_{c}{ }^{2}$ | $T_{\text {m }}$ | 0.990 | 4.7 |  |  |  |
| $\begin{aligned} & \text { MV }\left(\mathrm{cm}^{3}\right) \\ & n=69 \end{aligned}$ | $w_{\text {mad }}$ |  | 0.953 | 3.8 | ${ }^{0} x$ |  |  | 0.925 | 4.8 | I |  |  | 0.622 | 10.7 | $N_{\text {c }}$ |  |  | 0.974 | 2.8 | vol | 0.974 | 2.8 |
|  | $w_{\text {I }}$ |  | 0.982 | 2.3 | ${ }^{0} \chi$ | ${ }^{1} \chi$ |  | 0.965 | 3.3 | I | CIC |  | 0.964 | 3.3 | $N_{\text {c }}$ |  |  | 0.998 | 0.8 | area | 0.965 | 3.2 |
|  | $w_{\text {r }}$ | $f \quad p_{3}$ | 0.983 | 2.3 | ${ }^{0} x$ | ${ }^{1} \chi$ | ${ }^{3} \chi_{p}$ | 0.996 | 1.1 | I | CIC | SIC | 0.975 | 2.8 | $N_{\mathrm{c}}^{\mathrm{c}}$ | $p_{3}$ | $T_{\text {m }}$ | 0.999 | 0.6 |  |  |  |
| $\begin{aligned} & \text { MR }\left(\mathrm{cm}^{3}\right) \\ & n=69 \end{aligned}$ | $w_{\text {mod }}$ |  | 0.949 | 1.2 | ${ }^{0} x$ |  |  | 0.961 | 1.1 | 1 |  |  | 0.621 | 3.2 | $N_{\text {c }}$ |  |  | 0.998 | 0.2 | vol | 0.999 | 0.2 |
|  | $w_{\text {r }}$ | $f$ | 0.974 | 0.9 | ${ }^{0} x$ | ${ }^{1} \chi$ |  | 0.995 | 0.4 | I | CIC |  | 0.979 | 0.8 | $N_{\text {c }}$ | $p_{3}$ |  | 0.9999 | 0.06 | area | 0.993 | 0.4 |
|  | $w_{\text {r }}$ | $f \quad p_{3}$ | 0.990 | 0.5 | ${ }^{0} \chi$ | ${ }^{1} \chi$ | ${ }^{3} \chi_{p}$ | 0.999 | 0.1 | I | CIC | SIC | 0.998 | 0.2 | $N_{\text {c }}$ | $p_{3}$ | $T_{\mathrm{m}}$ | 0.9999 | 0.05 |  |  |  |
| $\begin{gathered} \mathrm{HV}(\mathrm{~kJ} / \\ \mathrm{mol}) \\ n=69 \end{gathered}$ | $w_{\text {mod }}$ |  | 0.949 | 1.2 | $\chi_{1}$ |  |  | 0.939 | 1.3 | I |  |  | 0.704 | 2.9 |  | $N_{\text {c }}$ |  | 0.918 | 1.6 | vol | 0.919 | 1.5 |
|  | $w_{r}$ |  | 0.994 | 0.4 | ${ }^{0} x$ | ${ }_{3}^{3} \chi_{6}$ |  | 0.974 | 0.9 | I | CIC |  | 0.917 | 1.6 | $N_{\text {c }}$ | $T_{\text {m }}$ |  | 0.983 | 0.71 | area | 0.888 | 1.8 |
|  | $w_{\text {r }}$ | $f \quad p_{3}$ | 0.994 | 0.4 | ${ }^{0} \chi$ | ${ }^{3} \chi^{\prime} \chi_{\text {c }}$ | ${ }^{4} \chi_{\text {c }}$ | 0.992 | 0.5 | I | CIC | ICM | 0.971 | 0.9 | $N_{\text {c }}^{\text {c }}$ | $T_{\mathrm{m}}$ | $p_{3}$ | 0.993 | 0.46 |  |  |  |
| $\begin{aligned} & \mathrm{TC}\left({ }^{\circ} \mathrm{C}\right) \\ & n=74 \end{aligned}$ | $w_{\text {mod }}$ |  | 0.814 | 24.9 | ${ }^{1} \chi$ |  |  | 0.933 | 14.9 | I |  |  | 0.660 | 33.6 | $N_{\text {c }}$ |  |  | 0.954 | 12.4 | vol | 0.954 | 12.4 |
|  | $w_{\text {r }}$ | $p_{3}$ | 0.965 | 10.9 | ${ }^{1} x$ | $1 / \chi_{\text {t }}$ |  | 0.982 | 7.8 | I | CIC |  | 0.902 | 18.2 | $N_{\text {c }}$ | $N_{\text {c }}{ }^{2}$ |  | 0.969 | 10.2 | area | 0.949 | 13.0 |
|  | $w_{\text {r }}$ | $p_{3} \quad 1 / w_{\text {r }}$ | 0.990 | 5.9 | ${ }^{1} \chi$ | ${ }^{4} \chi_{\text {pc }}$ | $1 /{ }^{1} x$ | 0.991 | 5.4 | I | CIC | SIC | 0.969 | 10.2 | $N_{\text {c }}$ | $1 / N_{\mathrm{c}}$ | $p_{3}$ | 0.984 | 7.4 |  |  |  |
| $\begin{aligned} & \mathrm{PC}(\mathrm{~atm}) \\ & n=74 \end{aligned}$ | $w_{\text {r }}$ |  |  |  |  |  |  | 0.904 | 1.3 | , |  |  | 0.613 | 2.7 |  |  |  | 0.870 | 1.6 | vol | 0.863 | 1.6 |
|  | $w_{\text {r }}$ | $f$ | 0.930 | 1.2 | $1 /{ }^{0} x$ | ${ }^{5} \chi_{p}$ |  | 0.955 | 0.9 | IC | CIC |  | 0.914 | 1.3 | $N_{\text {c }}$ | $p_{3}$ |  | 0.946 | 1.0 | area | 0.851 | 1.7 |
|  | $w_{\text {r }}$ | $f \quad 1 / w_{\mathrm{r}}$ | 0.957 | 0.9 | $11^{0} \chi$ | $1 / \chi_{t}$ | ${ }^{3} \chi_{p}$ | 0.967 | 0.8 | IC | CIC | ICM | 0.917 | 1.3 | $N_{\text {c }}$ | $p_{3}$ | $1 / N_{\text {c }}$ | 0.974 | 0.7 |  |  |  |
| $\begin{aligned} & \text { ST (dyne/ } \\ & \text { cm) } \\ & n=68 \end{aligned}$ | $p_{3}$ |  | 0.774 | 0.9 | $1^{1 / 2}$ |  |  | 0.832 | 0.8 | 1 |  |  | 0.490 | I. 4 | $1 / N_{\mathrm{c}}$ |  |  | 0.775 | 0.9 | vol | 0.775 | 0.9 |
|  | $w_{\text {r }}$ | $p_{3}$ | 0.954 | 0.4 | $1 / 1{ }^{1} \chi$ | ${ }^{3} \chi_{p}$ |  | 0.960 | 0.4 | IC | CIC |  | 0.784 | 0.9 | $1 / N_{c}$ | $p_{3}$ |  | 0.886 | 0.7 | area | 0.760 | 1.0 |
|  | $w_{\text {r }}$ | $f \quad p_{3}$ | 0.971 | 0.3 | $1 /{ }^{1} \chi$ | ${ }^{3} \chi_{p}$ | ${ }^{2} x$ | 0.970 | 0.3 | IC | CIC | ICM | 0.806 | 0.9 | $1 / N_{c}$ | $p_{3}$ | $T_{\text {m }}$ | 0.982 | 0.3 |  |  |  |
| $\begin{aligned} & \mathrm{mp}\left({ }^{\circ} \mathrm{C}\right) \\ & n=56 \end{aligned}$ | $f$ |  | 0.219 | 30.8 | $1 /{ }^{0} \chi$ |  |  | 0.243 | 30.4 | CIC |  |  | 0.104 | 33.0 | $1 / N_{c}$ |  |  | 0.229 | 30.6 | vol | 0.199 | 31.2 |
|  |  |  |  |  | $1 /{ }^{0} x$ | ${ }^{6} \chi_{c}$ |  | 0.370 | 27.9 | CIC | IC |  | 0.396 | 27.4 | $\mathrm{I} / N_{\mathrm{c}}$ | $T_{3}{ }^{2}$ |  | 0.290 | 29.7 | area | 0.212 | 31.0 |
|  |  |  |  |  | $1 /{ }^{0} \chi$ | ${ }^{6} \chi_{\text {c }}$ | ${ }^{4} \chi_{\text {c }}$ | 0.407 | 27.4 |  |  |  |  |  | $1 / N_{c}$ | $T_{3}$ | $T_{3}{ }^{2}$ | 0.367 | 28.3 |  |  |  |

Table VI. Multiple Regression Equations for the Physical Properties Using Connectivity Indices

$$
\begin{aligned}
\mathrm{bp}\left({ }^{\circ} \mathrm{C}\right)= & -9.6( \pm 4.1)+38.1( \pm 1.0)^{1} \chi-49.0( \pm 19.3) 1 /{ }^{0} \chi+5.7( \pm 0.3)^{4} \chi_{\mathrm{pc}}-94.5( \pm 9.8) \chi_{\mathrm{t}}+8.4( \pm 2.5)^{6} \chi_{\mathrm{p}} \\
& n=74, r^{2}=0.999, s=1.86, F=9030 \\
\mathrm{MV}\left(\mathrm{~cm}^{3}\right)= & 22.9( \pm 0.7)+14.6( \pm 0.2)^{0} \chi+16.2( \pm 0.4)^{1} \chi-7.3( \pm 0.2)^{3} \chi_{\mathrm{p}}-4.5( \pm 0.3)^{4} \chi_{\mathrm{p}}-2.1( \pm 0.3)^{5} \chi_{\mathrm{c}} \\
& n=69, r^{2}=0.999, s=0.5, F=14294 \\
\mathrm{MR}\left(\mathrm{~cm}^{3}\right)= & -0.8( \pm 0.1)+3.8( \pm 0.02)^{0} \chi+4.6( \pm 0.1)^{1} \chi-0.98( \pm 0.03)^{3} \chi_{\mathrm{p}}-0.63( \pm 0.04)^{4} \chi_{\mathrm{p}}-0.25( \pm 0.06)^{5} \chi_{\mathrm{p}} \\
& n=69, r^{2}=0.9999, s=0.05, F=152558 \\
\mathrm{HV}(\mathrm{~kJ} / \mathrm{mol})= & 1.9( \pm 0.3)+4.5( \pm 0.2)^{0} \chi+4.8( \pm 0.4)^{2} \chi-12.4( \pm 0.5)^{3} \chi_{\mathrm{c}}+20.7( \pm 0.8)^{4} \chi_{\mathrm{c}}+0.25( \pm 0.05)^{4} \chi_{\mathrm{pc}} \\
& n=69, r^{2}=0.998, s=0.2, F=7849 \\
\mathrm{TC}\left({ }^{\circ} \mathrm{C}\right)= & 150.7( \pm 9.8)+42.5( \pm 2.4)^{1} \chi+12.8( \pm 1.0)^{4} \chi_{\mathrm{pc}}-159.7( \pm 10.0) \chi_{\mathrm{t}}-11.5( \pm 3.3)^{5} \chi_{\mathrm{p}}-17.4( \pm 3.4)^{6} \chi_{\mathrm{c}} \\
& n=74, r^{2}=0.995, s=4.1, F=2795 \\
\mathrm{PC}(\mathrm{~atm})= & 30.6( \pm 0.6)+17.5( \pm 0.9) \chi_{\mathrm{t}}\left(\mathrm{k}_{\mathrm{c}}\right)-2.3( \pm 0.2)^{2} \chi+1.9( \pm 0.1)^{5} \chi_{\mathrm{pc}}-2.6( \pm 0.3)^{4} \chi_{\mathrm{p}}-1.4( \pm 0.4)^{6} \chi_{\mathrm{c}} \\
& n=74, r^{2}=0.981, s=0.6, F=694 \\
\mathrm{ST}(\mathrm{dyn} / \mathrm{cm})= & 31.3( \pm 0.7)-35.6( \pm 1.3) 1 / /^{1} \chi-0.8( \pm 0.1)^{2} \chi+0.8( \pm 0.1)^{3} \chi_{\mathrm{p}}+0.4( \pm 0.1)^{5} \chi_{\mathrm{pc}}+0.9( \pm 0.1)^{5} \chi_{\mathrm{c}} \\
\mathrm{mp}\left({ }^{\circ} \mathrm{C}\right)= & 39( \pm 33)-2192( \pm 652) 1 /{ }^{0} \chi+859( \pm 294) 1 /{ }^{1} \chi-94( \pm 22)^{3} \chi_{\mathrm{c}}+291( \pm 62)^{4} \chi_{\mathrm{c}}+77( \pm 21)^{6} \chi_{\mathrm{c}} \\
& n=56, r^{2}=0.570, s=23.8, F=13
\end{aligned}
$$

Table VII. Multiple Regression Equations for the Physical Properties Using ad Hoc Descriptors

$$
\begin{aligned}
\mathrm{bp}\left({ }^{\circ} \mathrm{C}\right)= & -152.9( \pm 3.4)+51.1( \pm 1.0) N_{\mathrm{c}}-16.0( \pm 1.5) T_{\mathrm{m}}+2.7( \pm 0.2) p_{3}-1.8( \pm 0.1) N_{\mathrm{c}}{ }^{2}+1.1( \pm 0.2) T_{\mathrm{m}}{ }^{2} \\
& n=74, r^{2}=0.998, s=2.0, F=7786 \\
\mathrm{MV}\left(\mathrm{~cm}^{3}\right)= & 6.8( \pm 4.0)+19.0( \pm 0.3) N_{\mathrm{c}}+62.1( \pm 13.5) 1 / N_{\mathrm{c}}+3.1( \pm 0.3) T_{\mathrm{m}}-0.33( \pm 0.04) T_{\mathrm{m}}{ }^{2}-1.81( \pm 0.04) p_{3} \\
& n=69, r^{2}=0.999, s=0.4, F=20452 \\
\mathrm{MR}\left(\mathrm{~cm}^{3}\right)= & 1.57( \pm 0.05)+4.78( \pm 0.01) N_{\mathrm{c}}-0.14( \pm 0.01) p_{3}+0.03( \pm 0.01) T_{\mathrm{m}} \\
& n=69, r^{2}=0.9999, s=0.05, F=267332 \\
\mathrm{HV}(\mathrm{~kJ} / \mathrm{mol})= & 6.6( \pm 0.5)+4.7( \pm 0.1) N_{\mathrm{c}}-1.95( \pm 0.07) T_{\mathrm{m}}+0.28( \pm 0.04) p_{3}+0.15( \pm 0.04) T_{3} \\
& n=69, r^{2}=0.994, s=0.4, F=2746 \\
\mathrm{TC}\left({ }^{\circ} \mathrm{C}\right)= & 77.5( \pm 38.3)+38.0( \pm 7.5) N_{\mathrm{c}}-1.3( \pm 0.4) N_{\mathrm{c}}{ }^{2}+6.3( \pm 0.4) p_{3}-6.7( \pm 0.7) T_{\mathrm{m}}-206.4( \pm 55.8) 1 / N_{\mathrm{c}} \\
& n=74, r^{2}=0.994, s=4.8, F=2074 \\
\mathrm{PC}(\mathrm{~atm})= & 40.7( \pm 1.5)+26.9( \pm 3.2) 1 / N_{\mathrm{c}}-2.9( \pm 0.2) N_{\mathrm{c}}+0.7( \pm 0.1) p_{3}-0.02( \pm 0.01) T_{3}{ }^{2}+0.04(+0.01) T_{\mathrm{m}}{ }^{2} \\
& n=74, r^{2}=0.978, s=0.7, F=594 \\
\mathrm{ST}(\mathrm{dyn} / \mathrm{cm})= & 28.1( \pm 0.5)-50.1( \pm 2.2) 1 / N_{\mathrm{c}}-1.7( \pm 0.2) T_{\mathrm{m}}+0.11( \pm 0.02) T_{\mathrm{m}}{ }^{2}+0.56( \pm 0.02) p_{3}+0.05( \pm 0.02) T_{3} \\
& n=68, r^{2}=0.989, s=0.2, F=1152 \\
\mathrm{mp}\left({ }^{\circ} \mathrm{C}\right)= & -70.2( \pm 10.5)-248.8( \pm 60.6) 1 / N_{\mathrm{c}}-12.6( \pm 5.0) T_{3}+2.4( \pm 0.8) T_{3}{ }^{2} \\
& n=56, r^{2}=0.367, s=28.3, F=10
\end{aligned}
$$

Table VIII. Estimates of the Relative Contributions of Molecular Mass, Branching, and Steric Factors to the Physical Properties ${ }^{a}$

| property | mass | branching | steric | error |
| :---: | :---: | :---: | :---: | :---: |
| bp | $+285.1(0.82)$ | $-44.5(0.13)$ | $+17.8(0.05)$ | 0.002 |
| MV | $+157.3(0.89)$ | $+6.7(0.04)$ | $-11.9(0.07)$ | 0.0006 |
| MR | $+37.5(0.97)$ | $+0.1(0.003)$ | $-0.9(0.02)$ | 0.0001 |
| HV | $+36.6(0.79)$ | $-7.6(0.16)$ | $+2.1(0.04)$ | 0.006 |
| TC | $+184.9(0.73)$ | $-26.1(0.10)$ | $+41.4(0.16)$ | 0.006 |
| PC | $-18.6(0.77)$ | $+0.6(0.02)$ | $+4.4(0.18)$ | 0.022 |
| ST | $-6.9(0.44)$ | $-4.8(0.31)$ | $+3.7(0.24)$ | 0.011 |
| mp | $-34.3^{b}(0.34)$ |  | $-2.8(0.03)$ | 0.633 |

${ }^{a}$ See text; fractional contributions shown in parentheses. ${ }^{b}$ Dependence on $1 / N_{c}$.
$82.5 \%$ of the variance in the properties examined. Addition of a second factor allows $94 \%$ of the property variance to be accounted for, and addition of a third factor allows almost $99 \%$ to be accounted for. When mp is excluded from the analysis ( 68 compounds), the first factor accounts for $92 \%$ of the variance in the remaining seven properties; a second factor allows over $98 \%$ of the variance in these seven properties to be reproduced.

Factor loadings from the PCA analysis are shown in Table X and Figure 1. These values represent correlations with the factors. With the exception of mp , the physical properties all are seen to load strongly on factor $f 1$. Factor $f 2$ is almost exclusively a melting point dimension; among the other properties only PC shows a significant loading on $f 2$. The third factor $f 3$ appears to be most significant for PC and ST and, to some extent, TC and mp. (In the seven-property ( 68 compounds) analysis with mp and hence $f 2$ excluded, factors $f 1$ and $f 3$ retain virtually the same loadings as in the full analysis; therefore, this latter factor structure is not shown.)

In the present analysis of the physical properties further orthogonal and oblique rotations of the axes did not lead to a simplification of the factor structure. It is known that such rotations can often yield results that are not physically meaningful. ${ }^{53}$

[^6] Sci. 1979, 19, 19.

Table IX. Results of Principal Component Analysis for the Physical Properties: Eigenvalues and, in Parentheses, Cumulative Percent Variance Reproduced

| factors | $\delta$ properties <br> $(51$ compounds $)$ | 7 properties <br> $(68$ compounds $)$ |
| :---: | :---: | :---: |
| $f 1$ | $6.598(82.5)$ | $6.442(92.0)$ |
| $f 2$ | $0.921(94.0)$ | $0.451(98.5)$ |
| $f 3$ | $0.378(98.7)$ | $0.088(99.7)$ |
| $f 4$ | $0.089(99.8)$ | $0.013(99.9)$ |
| $f 5$ | $0.011(99.97)$ | $0.004(99.97)$ |
| $f 6$ | $0.002(99.99)$ | $0.002(99.99)$ |
| $f 7$ | $0.0008(100)$ | $0.0004(100)$ |
| $f 8$ | $0.0003(100)$ |  |

Table X. PCA Factor Loadings for the Physical Properties

|  | PCA factor loadings |  |  |
| :---: | ---: | ---: | ---: |
| property | $f 1$ | $f 2$ | $f 3$ |
| bp | 0.996 | -0.011 | 0.079 |
| MV | 0.967 | -0.149 | -0.161 |
| MR | 0.983 | -0.092 | -0.058 |
| HV | 0.983 | -0.065 | 0.042 |
| TC | 0.974 | 0.064 | 0.195 |
| PC | -0.876 | 0.269 | 0.377 |
| ST | 0.925 | 0.131 | 0.343 |
| mp | 0.406 | 0.890 | -0.207 |

It was of interest to attempt to model the factors arising from the factor analysis in order to assess their physical significance. $f 1$ was strongly correlated ( $r^{2}=0.968$ ) with the calculated molecular volumes, $V_{\mathrm{B}}$. In terms of the ad hoc descriptors and connectivity indices, eq 6 and 7 were found.

$$
\begin{gathered}
f 1=-6.60( \pm 0.08)+0.92( \pm 0.01) N_{\mathrm{c}}-0.20( \pm 0.02) T_{m}+ \\
0.007( \pm 0.001) T_{3}^{2}(6) \\
n=51 \quad r^{2}=0.993 \quad s=0.08 \\
f 1=2.8( \pm 0.4)-13.7( \pm 0.9) 1 /{ }^{1} \chi+0.15( \pm 0.02) 1 / \chi_{1}+ \\
0.19( \pm 0.02)^{4} \chi_{\mathrm{pc}}(7) \\
n=51 \quad r^{2}=0.988 \quad s=0.1
\end{gathered}
$$

Table XI. Summary of Principal Component Analysis for the Parameter Sets ${ }^{a}$

|  | connectivity <br> indices | Wiener <br> indices | ad hoc <br> descriptors | information <br> indices |
| :--- | :--- | :--- | :--- | :--- |
| $f 1$ | $8.745(48.6)$ | $5.187(74.1)$ | $4.918(61.5)$ | $4.550(91)$ |
| $f 2$ | $4.712(74.8)$ | $0.981(88.1)$ | $2.102(87.8)$ | $0.418(99.4)$ |
| $f 3$ | $1.556(83.4)$ | $0.642(97.3)$ | $0.534(94.4)$ | $0.027(99.9)$ |
| $f 4$ | $1.276(90.5)$ | $0.156(99.5)$ | $0.269(97.8)$ | $0.005(99.99)$ |
| $f 5$ | $0.672(94.2)$ | $0.032(99.98)$ | $0.108(99.1)$ | $0.0003(100)$ |
| $f 6$ | $0.448(96.7)$ | $0.001(100)$ | $0.059(99.9)$ |  |
| $f 7$ | $0.279(98.3)$ | $0.00003(100)$ | $0.008(99.98)$ |  |
| $f 8$ | $0.166(99.2)$ |  | $0.001(100)$ |  |
| $f 9$ | $0.074(99.6)$ |  |  |  |
| $f 10$ | $0.035(99.8)$ |  |  |  |

${ }^{a}$ Eigenvalues (percent variance reproduced).
In contrast, $f 2$ is entirely unrelated to $V_{\mathrm{B}}\left(r^{2}=0.006\right)$. Its equations are dominated by shape-dependent terms and higher order cluster terms (eq 8 and 9).

$$
\begin{gathered}
f 2=2.8( \pm 1.4)+0.04( \pm 0.01) T_{3}^{2}-1.4( \pm 0.8) T_{m}+ \\
0.2( \pm 0.1) T_{m}{ }^{2}(8) \\
n=51 \quad r^{2}=0.303 \quad s=0.9 \\
f 2=1.6( \pm 0.6)+3.4( \pm 0.7)^{6} \chi_{\mathrm{c}}-0.6( \pm 0.2)^{2} \chi+ \\
2.0( \pm 1.0)^{4} \chi_{\mathrm{c}}(9) \\
n=51 \quad r^{2}=0.414 \quad s=0.8
\end{gathered}
$$

Factor $f 3$ is also unrelated to $V_{\mathrm{B}}\left(r^{2}=0.001\right)$. Its equations show influences from both mass- and path-dependent terms (eq 10 and 11).

$$
\begin{gathered}
f 3=0.47( \pm 0.26)+0.61( \pm 0.05) p_{3}-0.056( \pm 0.006) N_{\mathrm{c}}^{2}- \\
0.05( \pm 0.01) T_{m}^{2}(10) \\
n=51 \quad r^{2}=0.784 \quad s=0.5 \\
f 3=-0.5( \pm 0.3)+1.7( \pm 0.1)^{3} \chi_{p}-0.28( \pm 0.04) 1 / \chi_{\mathrm{t}}- \\
0.7( \pm 0.1)^{3} \chi_{\mathrm{c}}(11) \\
n=51 \quad r^{2}=0.785 \quad s=0.5
\end{gathered}
$$

It is also possible to apply PCA to the parameter sets used for these $\mathrm{C}_{2}-\mathrm{C}_{9}$ alkanes. The results are shown in abbreviated form in Table XI. Application of several criteria noted under Methods indicates that in terms of their major variances the Wiener indices span 3 dimensions, the connectivity indices, 6 or 7 dimensions, the information indices, 2 dimensions, and the ad hoc descriptors, 3 or 4 dimensions.

## Discussion

The regression equations in Tables VI and VII provide a basis for the estimation of missing values for most of the physical properties examined here. For most properties except mp the accuracies of the equations should be sufficient for many practical purposes. The equations reflect the degree to which each property can be represented in an additive/constitutive manner based on the present descriptors.

The ad hoc descriptor equations (Table VII) display the relative influences of molecular mass $\left(N_{\mathrm{c}}\right)$, branching ( $T_{\mathrm{m}}$ ), and steric factors $\left(T_{3}, p_{3}\right)$. Clearly, mass is overwhelmingly the dominant influence. Branching and steric differences cause smaller alterations in the average intermolecular distances and corresponding alterations of the intermolecular forces. ${ }^{15}$ Branching, e.g., sequesters parts of the molecule and thereby prevents close contact with neighboring molecules. Since intermolecular interaction energies fall sharply as $1 / r^{6}$, this decreases the cohesive forces experienced by such molecules. Steric crowding causes a small reduction in the molar volume (see the negative coefficient for $p_{3}$ in the MV expression). Therefore properties such as bp, HV, TC, and ST, which depend directly on the strength of intermolecular forces, tend to display positive dependences on $N_{\mathrm{c}}$, negative dependences on $T_{m}$, and positive dependences on $p_{3}$ or $T_{3}$. As a rule-unless they are dominant in magnitude-the quadratic and inverse terms account for nonlinear dependences and may take
either sign. The critical pressure (PC) decreases as the intermolecular forces increase and shows a negative dependence on $N_{\mathrm{c}}$ (its much smaller dependences on $p_{3}$ and $T_{3}$ do not follow this pattern). The signs and relative magnitudes of these influences are more completely illustrated in Table VIII.

The failure of the present parameters to model the melting points of these hydrocarbons is not surprising and demonstrates the greater subtlety of the melting transition compared to, e.g., the boiling and the critical transitions. ${ }^{15,22}$ The latter processes depend, in a more or less straightforward manner, on complete disruption of intermolecular forces and thus on the strengths of these forces. Conversely, the melting transition maintains a condensed phase and involves disruption of specific intermolecular fits and geometric arrangements that lie beyond the scope of the present parameters. Results of the factor analysis further emphasize this distinction and show melting to lie on a dimension almost entirely independent of the other properties. Modeling of this dimension (eq 8 and 9) shows it to depend on shape-dependent, as contrasted to mass-dependent, terms. In some cases a comparative approach has been used in treating melting points. ${ }^{54}$ Recently, Hanson and Rouvray ${ }^{55}$ have reviewed studies of melting points and achieved successful correlations with topological indices for normal alkanes. They indicate that their method can be extended also to the branched alkanes. ${ }^{56}$ Kier ${ }^{57,58}$ has recently described shape indices that hold promise for the description of melting points. ${ }^{59}$

All four structural parameter sets tested were reasonably successful in accounting for the physical properties of these alkanes, but the connectivity indices and ad hoc descriptors generally provided the most accurate models (Table IV). In part, this reflects the greater numbers of parameters in these two sets. Nonetheless, we conclude that these latter indices form well-chosen sets of structural descriptors with which to account for the physical properties of the normal and branched alkanes. When developing the form of the molecular connectivity index, Randic emphasized that this form was a solution to the bond-ordering problem for physical properties. ${ }^{20,60}$ In a comparison of six topological indices, Razinger et al. ${ }^{61}$ found the connectivity index to be the most effective in representing several properties of the alkanes. The success of connectivity indices in the present example and in an enormous variety of other applications ${ }^{8-10,13-15,20,22,41,62,63}$ speaks strongly for the form chosen. This view is reinforced by the factor analysis, which reveals that the connectivity indices and ad hoc descriptors span more major, independent dimensions than do the other parameter sets. Although it must be emphasized that a parameter set with more major dimensions will not necessarily contain dimensions physically relevant to a set of properties, ${ }^{64}$ a priori a set with more dimensions may be expected to have a better chance of containing these relevant dimensions than a set with fewer dimensions. As an initial condition, a parameter set should contain at least as many dimensions as do the properties to be modeled (here two or three) in order to have a good chance of success. In a relevant study Basak et al. have examined 90 topological indices using PCA on a diverse data set of 3692 structures and found 10 significant principal components. ${ }^{50}$

Recently, attention has turned to the use of alternative expressions, such as the Walker form ${ }^{65}$
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$$
\begin{equation*}
\text { property }=a[\text { index }]^{b} \tag{12}
\end{equation*}
$$

where $a$ and $b$ are coefficients to be determined, in structureproperty analysis. Rouvray and Pandey ${ }^{66}$ have employed the Wiener index and Walker expressions in an analysis of the boiling points of normal alkanes. They found different dependences for the lower and higher molecular weight alkanes, which they attributed to the effects of folding in the longer chains. Similar arguments have appeared in other contexts. ${ }^{67}$ In the multiple linear regression analysis, these longer chain effects are represented to some extent in the nonlinear terms such as $1 / N_{\mathrm{c}}$ and $N_{c}{ }^{2}$ and by $p_{3}$ and higher order path terms.

In the present study, limited to the physical properties of a class of nonpolar compounds, a single major factor was dominant for seven of the eight properties examined (Table IX). The most reasonab e interpretation of this factor is as a mass- or bulk-related dimension associated with intermolecular dispersion forces. This interpretation is consistent with the strong correlation of this factor with molecular volume ${ }^{68}$ and with its expansion in terms of ad hoc descriptors and connectivity indices (eq 6 and 7). It is also reflected in the $f 1$ factor scores (not shown ${ }^{69}$ ), which are most negative for the lower molecular weight, branched compounds and most positive for $n$-nonane and several lightly branched nonanes. Meyer and co-workers ${ }^{70,71}$ have shown that dispersion forces dominate the liquid properties even of relatively polar compounds, and such forces are surely of overwhelming importance for the alkanes examined in the present investigation. A second factor, associated with the melting points, is correlated with features of molecular shape and steric fit (eq 8 and 9). This factor is only of minor importance for properties other than mp. A third factor, independent of molecular volume and difficult to characterize otherwise, appears to account for a smaller fraction of the property variances not represented in the first two factors.

In an important study of the physical properties of a diverse set of 114 compounds, Cramer ${ }^{47}$ used PCA to identify two major dimensions, which he termed $B$ and $C$, and three minor dimensions, termed $D, E$, and $F$, for the properties. The major dimensions $B$ and $C$ accounted for about $96 \%$ of the variance in six of the properties. Cramer associated dimension $B$ with "some aspect of molecular bulk". The largest molecules in the set had the highest $B$ scores, and the smallest, the lowest $B$ scores. $C$ was identified as a polar dimension related to molecular "cohesiveness;" because of the orthogonality of the PCA axes, this second axis was more exactly described as cohesiveness relative to the given molecular bulk. ${ }^{47}$ Dimension $D$ was associated with "dispersion interactions" and molecular "deformability", and dimensions $E$ and $F$, with minor, ideosyncratic aspects of molecular behavior.

[^7]Cramer also applied these concepts to a set of 139 additional compounds and derived additive-constitutive models permitting calculation of the factor scores from molecular structure. ${ }^{47}$

On the basis of the present results and an examination of Cramer's results, we offer the following reinterpretation of Cramer's dimensions in terms of physical interactions. The bulk dimension $B$ is clearly a measure of molecular dispersion interactions. As noted by Cramer, $B$ is strongly associated with molecular mass/volume, a feature typical of dispersion interactions. Cramer's linear fragment model for calculation of molecular $B$ values is entirely consistent with this; e.g., the values for atoms $\mathrm{H} \approx \mathrm{F}<\mathrm{Cl}<\mathrm{Br}<\mathrm{I}$ are in the order of the atomic polarizabilities. Even the negative dependence on alkane branching noted in our work is reflected in Cramer's alkane $B$ scores. The fundamental dependencies on $B$ of the physical properties are also typical of dispersion interactions (cf. Table VI of ref 47 and our Table VIII). Thus, Cramer's $B$ dimension corresponds to the major dimension found in the present study. We see no compelling reason to associate Cramer's minor $D$ dimension with dispersion interactions, although this dimension may represent a minor adjustment to either the $B$ or $C$ dimensions. $C$ is certainly a "polar cohesiveness" measure, but it is dominated by hydrogen-bonding contributions. The most positive $C$ values in the original compound set occur for acetamide, water, acetic acid, methanol, and ethanol-all strong hydrogen-bonding agents; the most negative $C$ values are for branched hydrocarbons, such as 2,2-dimethylbutane. Of the additional 139 compounds examined by Cramer, glycerol, hydrazine, and ammonia have the most positive $C$ values, and hexadecane has the lowest. This influential hydrogen-bonding component is also reflected in Cramer's linear fragment model ${ }^{47}$ for $C$ where the largest positive contributions are from $-\mathrm{OH},-\mathrm{CN}$, $>\mathrm{C}=\mathrm{O}$, and $-\mathrm{NH}_{2}$ groups. This polar, hydrogen-bonding dimension is necessarily absent from our present analysis of the alkanes.

In conclusion, we have applied graph-theoretical molecular modeling techniques to eight representative physical properties of the linear and branched alkanes through the nonanes. With the notable exception of the melting points, connectivity indices and ad hoc descriptors are found to be very useful parameter sets for modeling these properties. Factor analysis reveals that most of these properties are dominated by a single mass/volume-related dimension, reasonably associated with intermolecular dispersion interactions. Melting points are associated with a shape-dependent dimension not well modeled by the indices examined.

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[^4]:    ${ }^{a}$ Units are the following: bp, ${ }^{\circ} \mathrm{C} ; \mathrm{MV}, \mathrm{cm}^{3} / \mathrm{mol}$ at $20^{\circ} \mathrm{C} ; \mathrm{MR}, \mathrm{cm}^{3} / \mathrm{mol}, \mathrm{HV}, \mathrm{kJ} / \mathrm{mol} ; \mathrm{TC},{ }^{\circ} \mathrm{C} ; \mathrm{PC}$, atm; ST, dyn/cm; mp, ${ }^{\circ} \mathrm{C}$. ${ }^{b} \mathrm{Abbreviations}$

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